C3. Dead Loads

C3.2 Weights of Materials and Constructions. To establish uniform practice among designers, it is desirable to present a list of materials generally used in building construction, together with their proper weights. Many building codes prescribe the minimum weights for only a few building materials, and in other instances no guide whatsoever is furnished on this subject. In some cases the codes are so drawn up as to leave the question of what weights to use to the discretion of the building official. without providing any authoritative guide. This practice, as well as the use of incomplete lists, has been subjected to much criticism. The solution chosen has been to present, in this commentary, an extended list that will be useful to designer and official alike. However, special cases will unavoidably arise, and authority is therefore granted in the standard for the building official to deal with them.

For ease of computation, most values are given in terms of pounds per square foot (lb/ft²) (kN/m²) of given thickness (see Table C3-1). Pounds-per-cubic-foot (lb/ft³) (kN/m³) values, consistent with the pounds-per-square foot (kilonewtons per square meter) values, are also presented in some cases (see Table C3-2). Some constructions for which a single figure is given actually have a considerable range in weight. The average figure given is suitable for general use, but when there is reason to suspect a considerable deviation from this, the actual weight should be determined.

Engineers, architects, and building owners are advised to consider factors that result in differences between actual and calculated loads.

Engineers and architects cannot be responsible for circumstances beyond their control. Experience has shown, however, that conditions are encountered which, if not considered in design, may reduce the future utility of a building or reduce its margin of safety. Among them are:

- Dead Loads. There have been numerous
 instances in which the actual weights of members
 and construction materials have exceeded the
 values used in design. Care is advised in the use
 of tabular values. Also, allowances should be
 made for such factors as the influence of
 formwork and support deflections on the actual
 thickness of a concrete slab of prescribed
 nominal thickness.
- 2 Future Installations, Allowance should be made for the weight of future wearing or protective surfaces where there is a good possibility that such may be applied. Special consideration should be given to the likely types and position of partitions, as insufficient provision for

partitioning may reduce the future utility of the building

Attention is directed also to the possibility of temporary changes in the use of a building, as in the case of clearing dormitory for a dance or other recreational purpose

Table C 3-1; Minimum Design Dead Loads*

		DRO'		1700					
Confection of the content part of the conten	Component	(Ist)	Component	(Jsd)	ŏ	mposent			
1. Carlot Greater, get with the content of the co	CELANGS		FLOOR TIEL.		Chy brick wythes				
4 Study Species 2	Acoustical Fiber Board	-	Cinder concrete, per inch	6	· fui				39
Similar of the control of the cont	Gypsum board (per mm thickness)	0.55	Lightweight concrete, per inch	00	8 in.				19
Storet Control (1997) Stor	Mechanical duet allowance	77	Sand, per inch	80	12 in.				115
## \$10,000 KOUR DECORATIONS A Considered south by Notes, and a considered south by Notes, and A Considerate of the Considered south by Notes, and A Considerate of the Considerate of	Pluster on tile or concrete	~	Stone concrete, per inch	13	16 in.				155
Converted filtring to a particular state of the converted filtring filtring to a particular state of the converted filtring state of the converted filtring filtring filtring filtring state of the converted filtring	Plaster on wood Inth	œ	FLOORS AND FLOOR FINISHES						
1. Counse from the first bit of more connected in the first bit of the counse from the first bit of the fir	Suspended steet channel system	7	Asphalt block (2-u.), 1/2-in maxum	30	Hollaw concrete masonry mil wyth	ies.			
Second content of the Connection of the Connec	Suspended ment hath and ecovera plaster	13	· Cement fluish (1-in) on snanc-concrete fill	35	Wythe thickness (in inches)				
13 Concate of Humbridge State 13 14 15 15 15 15 15 15 15	Suspended metal lath and gypsom plaster	91	Ceramic or sprarry file (3/4-in) on 1/2-in, sportar bed	91	Density of and (16 49 kN/m²)				
1	Wood furning suspension system	2.5	Ceramic or quarry tile (3/4-in.) on 1-in morns hed	23	No grout	7			
1 13 13 14 16 15 15 15 15 15 15 15	COVERINGS, ROOF, AND WALL		Concrete fill finish (per inch thickness)	12.	48"00.		2		55
1. Mainte and attained as a source-consecret lift 1. 1. 24 1. 1. 1. 1. 1. 1. 1. 1	Asbestos centent stringles	4	Hardwood Booring, 177-in.	4			Ж.		
15 Maintenant training and another control of the first of the fir	Asphalt shingles	2	Lineteum or asphalt tile, 1/4-in	-			37		
13 Solice flow that the class 15 16 0.0 c. 16 17 18 18 18 18 18 18 18	Cement tile	119	Mathe and mental en stone-concrete litt	3.5			æ		
1.2. Social data (a. 1.2. 1.2.	Clay life (for mortar add 10 psf)		Slate (per som thickness)	<u> </u>	16" 9.6.		Ţ		
10	Book tile, 2-in.	12	Solid flat tile on tin mortar base	2.3	Full Grout		23		
10 Terranzo (Link) discretely on sub-based on the state of the sta	Book life, 3-in	30	Subflooring, 3/4-in.	m					
12 Ternazo (1 m) and sone concept 11 12 m sone concept 13 14 14 14 14 14 14 14	Ludowici	01	Terrazzo (1-1/2-in.) directly on stab	19	Density of unit (125 pef):				
19 Territor (1 m) 2 to 2 to 4 month of the control (1 m) 2 to 4 month of 1 month of	Routan	13	Terrazzo (1-in.) on stone-concrete fill	32	No grant	2			
Wond black Unity on warrie, and fill 10 40° or quiville 10 45° or quiville 10 40° or quiville 10 45° or quiville 10° or quiville 10	Spanish	19	Terrazzo (1-in.), 2-in. stone concrete	32	48" o c.		3		
1 Words March Using manner base 14 Words March Using manner base 15 Words Word	Composition:		Wood block (3-in) on marrie, no fill	al			ň		
1 DOUBLE WOOD FLORE IN PLASE IN 1 DOUBLE WOOD FLORE IN 1 DOUBLE WOOD FLORE IN 2 Market Wood State 1 1 1 1 1 1 2 Market Wood State 2 4 4 4 4 4 4 4 4 2 Market Wood State 2 4 4 4 4 4 4 4 4 4	There ply vendy incling	-	Wond block (3-in) on 1/2-in morner base	3,6	•		Ä		
1	Four-ply felt and gravel	\$.5	FLOORS, WOOD-JOIST (NO PLASTER)				Ä		
1	Five-ply felt and gravel	Ş	DOUBLE WOOD FLOOR		16. o.c.		÷		
1	Copper or tin	-		d-in.	Full Grout		3		_
1	Corrugated asbestos-coment roofing	ų.	Smooth Business	acing					
3 2 × 16 6 5 5 44° 0¢ 7 10 17 18 18 18 18 18 18 18	Deck, meint, 20 gage	7.5	(1970) (1970)	LAN.	Deusity of unit (21.2) kN/m3				
Automate	Deck, metal, 18 gage	æ.	9	٠.	Nogrous	1			
10	Decking, 2-in-wood (Donglas fir)	ç	9	\$	48" o.c.		ž		
1	Decking, Jan word (Danglas fic)	æ	7	ۓ			*		
1	Fiberboard, 112-in	0.75	20	9	üs		38		
Move place street partitions 4 16° n c 46 61 76 10	Gypsum sheathing, 1/2-in.	3	FRAME PARTITIONS		24" p.e.		₹		
11 Wood studs, 1/2-in gypsum board each sade B Full Groud 4	Insulation, roof boards (per inch thickness)		Movable steel partitions	-7	16"0 c.) ;		
1.1 Wood study, 2 x 4, unphastered 1.2 Solid concrete masonry unit wellies (incl. 1.2 Wood study, 2 x 4, plastered one side 1.2 Solid concrete masonry unit wellies (incl. 1.3 1.3 1.4	Cellular glass	0.7	Wood or steet studs, 1/2-in gypsum board each side	20	Full Grout				
15 Wood study, 2 x 4, plastered one side 12 Solid concrete masonity unit wythes (incl.) 0.8 Wood study, 2 x 4, plastered two sides 20 Wythe thickness (in mm) 32 51 69 87 0.2 FRAME WALLS Density of mm (103 pcg). 32 51 69 87 102 0.5 Exterior stud walts. 12 Density of unit (123 pcf). 41 64 87 110 0.75 2 x 6 (@ 16-in., 58-in. gypsum, insulated, 3/8-in. sidny 48 8 Exterior stud walts with brick vencer 8 10 3 48 8 7 Windows, glass, frame and sush 3 5 15 40	Fibrous glass	Ξ	Wood studs, 2 x 4, unplastered	4					
0.2 Wydre thickness (in nm) 4 6 8 10 0.2 FRAME WALLS Density of unit (105 pcg). 32 51 69 87 0.2 Exterior stud walls: Density of unit (105 pcg). 38 60 81 102 0.75 2 x 6 (@ 10-in, 5/8-in gypsum, insulated, 3/8-in siding. 12 Density of unit (125 pcf). 41 6.4 87 110 0.75 2 x 6 (@ 10-in, 5/8-in gypsum, insulated, 3/8-in siding. 12 Density of unit (125 pcf). 41 6.4 87 110 10 Windows, glass, frame and sish. 3 3 3 5 1.5 Windows, glass, frame and sish. 3 3 3 110 0.7 Windows, glass, frame and sish. 3 3 3 3 3 1.5 3 3 3 3 3 3 3 4 6 8 110 1.5 3 3 3 3 3 4 6 8 110 4 6 8 110 4 6 8 110	Fiberboard	15	Wood studs, 2 x 4, plastered one side	7	Solid concrete masonry unit wyther	: (incl.			
0.2 FRAME WALL.S Density of min (105 pcg). 32 51 69 87 0.5 Exterior stud walks. Density of min (125 pcf). 38 60 81 102 0.4 2 x 4 @ 10 cm., 5/8-in gypsum, insulated, 3/8-in stding. 12 Density of min (135 pcf). 41 64 87 110 10.5 2 x 6 @ 16-in, 5/8-in gypsum, insulated, 3/8-in stding. 12 8 8 110 10 Windows, glass, frame and snsh. 3 3 5.5 1.5 3 1.5 1.0 1.5 1.0 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 2.5 1.5 3 3 3 3 3 3 3 3	Perlite	B 0	Wood stude, 2 x 4, phystered two sides	26	Wythe thickness (in mm)				
Density of unit (125 pcf) 38 60 81 102	Polystyrene foam	0.2	FRAME WALLS		Density of mit (105 pcg).	•			
0.4 2 x 4 @ 16-in, 5/8-in gypsum, insulated, 3/8-in siding i.1 Density of min (135 pcf). 41 64 87 110 0.75 2 x 6 @ 16-in, 5/8-in gypsum, insulated, 3/8-in siding 12 8 Exterior stud walls with brick verteer 8 7 Windows, glass, frame and snsh 3 5.5 1.5 1.7 1.7 1.7 2.8 3.7 3.3 3.3 3.3 3.3 3.4 3.4 4.6 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7	Urethane foam with skin	0.5	Exterior stud walks:		Density of unit (125 pcf):				
0.75 2 x 6 @ 16-in ,5/8-in gypsum, insulated, 3/8-in sidning 8 Exterior stud walls with brick verteer 7 Windows, glass, frame and sash 10 1 5 1 5 3 3	Plywood (per 1/8-in thickness)	0.4	2 x 4 @ 16-in., 5/8-in. gypsum, insulated, 3/8-in siding	==	Density of unit (135 pef):	4			
155 B Exterior stud walls with brick vencer 7 Windows, glass, frame and sash 10 5.5 1.5 1.5 1.3 3.3	Rigid insulation, 1/2-in	0.75	2 x 6 @ 16-in 5/8-in gypsum, insulated, 3/8-in. siding	12					
7 Windows, glass, frame and snsh 10 5.5 1.5 1.5 0.7 3.3	Skylight, metal frame, 3/8-in, wire glass	œ	Exterior stud walls with brick vencer	48					
6.5 5.5 1.3 1.0 0.7 0.7 3.3	Slate, 3/16-in.	7	Windows, glass, frame and sash	60					
5.5 1.5 1.0 0.7 0.7 3.3	Slate, 1/4-in.	10		r					
5.5 1.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	Wateproofing membranes:			1.					
	Branninous, gravel-covered	\$.5							
	Bitummous, smooth surface	1.5							
	Liquid applied	-							
Woud steathing (per inch trickness) 3 3 Wood stringles 3 3	Single ply, sheet	6.7							
Wood shingles 3	Wood sheathing (per inch thickness)	~							
	Wood shingles	М							

^{*} Weights of masoury include mortar but not phaster. For phaster, add 5 lb/lt? for each face phastered. Values given represent averages. In some cases there is a considerable range of weight for the same construction.

Loads*	
Dead	
Design	1
Minimum	
C 3-1:	
able (

					9.00								
Component	Lond (kN/m²)		Component	ent		Load (kN/m²)		Com	Component				(FN/H)
CETEINGS		11 008 1111.					Clay brick werkes	vrhes					
Acoustical Fiber Board	0.05	Coult concerte, per min	=			0.017	102 mm						- 87
Gypsum board (per min thickness)	8000	Lightweight concrete per mm	le per mm			0 0 1 5	203 mm						3.78
Mechanical duct allowance	610	Sand, per min				0015	305 (1)						5.51
Pinster on tile or concrete	P2 0	-	permin			F\$0.0	406 ann						, 42
Plaster on wood Jath	Br 0	FLOORS AND LLOOR I INISHI \$	JOR I INISEL S										
Suspended steel channel system	01 0	Asphalt block (51 mm), 13 mm modes	ւտ), Լ3 ատ տօժու			-	Hallow conc	Hollow concrete masons, unit wythes	so				
Suspended metal ladi and cement plaster	77.0	Cement finish (25 n	Cement finish (25 mm) on stone concrete till	ie fill		151	Wythe thick	Wythe thickness (m.mm)	102	251	201	5.24	101
Suspended ment fail and gypsum plaster	() 48	Cermine or quary t	Cermine or quarry tile (19 mm) on 13 mm mortar had	m worten had		0.77	Density of a	Density of mat (16 49 kN/m²)					
Wood furing suspension system	0 12	Ceramic or quarry 1	Ceramic or quarry tile (19 mm) on 25 mm mortor bud	m moran bud		01	No grout		=	1.2	3	10.7	::
COMPONICE BODS, AND WALL	1	Come to fill fourth from the force	town that farmers			נטט	0119			#F	(0.1	1 16	** (
COVERINGS MAKE, MINI WALL		Control of the small	per titili titickilessy		•	1700	URUL 2.171			9 ;	7		
Asbustov-coment shingles	í n	Hardwead Boering 72 mm	72 mm			<u>?</u>	(016 mm			<u>-</u>	ŝ,	<u>-</u>	=
Asphalt shingles	010	I moteum or asphalt life, 6 mm	nle, 6 mm			0.05	80 June	Sharing		<u> </u>	~	Š	<u>-</u> -
Cementale	0 77	Marbie and mortar o	Madble and mortar on stone-concrete full	_		1.58	640 mm			177	3.11	7 02	<u>.</u>
Clay tile (for mornin add 0 15kN/m²)		Slute (per mm thickness)	1055)			87 d O	IU0 IIII			2.01	2 68	1.15	
Book tile, 51 man	0.57	Solid that tile on 25 intra mortan base	ath montai base			01 -	Ind Groun			17.7	169	691	5.70
Rock tile 76 mm	96 0	Subflooring 19 mm				0 14							
Ladound Company	200	forman (38 mm) threathy an elab	dela no ottom			- 60	Demonstra	Density of ann (125 och					
	2.0	Tecretic (36 mm)	Terreto (36 mm) and the control of			: 5	Mo mon	(a d - a c)	1.75	2	77	7 11	2.19
Kunan	600	C 1000 (2) 02200151	t sione contacte mi								! =	; ;	
Spanish	- K	(time c7) 0/28401	Lerrazzo (25 mm), 51 mm stone concrete	e		55	mm 5171			-	117	667	,,,
Сопрознен		Wood block (76 mm) on mastic, no fill	a) on massic, no fill			0 48	1016 mm	growt		163	5 5	2 68	=
Flirec-pfy read, toofing	0 05	Wood block (76 mm	Wood block (76 mm) on 13 mm morter base	base		0.77	813 ann	spacing		1 72	3 25	2 78	326
four-ply felt and gravel	920	FLOORS, WOOD-J	FLOORS, WOOD-JOIST (NO PLASTER)	€.			610 mm			187	2 44	3 02	3.59
i sve-oly felt and gravel	0 29	DOUBLE WOOD 11 DOR	1 00R				406 11111			2.11	2 78	3 50	417
Concer of the	000		305 mm	406 mm	610 mm		1 all Grou			2 82	3 88	4 88	5.89
Corrors to despectors of the	61.0	loret ergos	mar vens	2007	JIDI WUS								
COLUMNICA ASOCSIOS-COLUMNICA COLUMNICA	2 0	(mm)	Stringle (Landy)	of Miles	e de la constanta		13	(Author) (2) 21 (Albush)					
ofen and an analysis of the second analysis of the second analysis of the second and an analysis	7 - 0	(14111)	(AINTHE)	(myym)	(Kiwille)		Lichard of F	(117, 17 17 17 17 17 17 17 17 17 17 17 17 17	05 -	071	-	9	101
Deck, metal, 18 gage	-	761 × 16	670	770	67.0		No groun		66 -	90	2 9	66.7	7 .
Decking, 51 mm wood (Dougles fir)	12 0	SI x 203	0 2 9	0 29	0 24		1219 mm			- %	5 39	2 92	-
Decking, 76 mm wood (Douglas fir)	0.38	51 x 254	0 34	67 0	62 P		1016 mm	groud		172	2 54	==	9 (9
Fiberboard, 13 mm	0 04	51 x 305	0.38	0.34	62 0		MIT IN	Smords		1 82	5 63	3 76	383
Gypsum sheathing, 13 mm	010	FRAME PARTITIONS	SNS				610 mm			1 96	2 82	3 50	4 12
Insulation, roof boards (per mm thickness)		Movable steel partitions	\$1101			610	406 mm			2.25	3 16	3.93	4 69
Cellular glass	1000	Wood or steel study	Wood or steel study, 13 mm gypsynn board each side	and cach side		80.0	Full Groun	_		3 06	4 17	\$ 27	6.17
sala suosti i	0 0021	Wood studs, \$1 x 102, unplastered	02, unphasicred			0 19							
Liberhaard	0 0028	Wood studs 51 x 13	Wood studs 51 x 102, plastered one side	v		0 57	Solid concre	Solid concrete masonry unit wythes (mel	mel				
Dorling	0.0015	Wood studs 51 x 16	Wood studs 51 x 102 plastered two sides	cs		960	Wythe thicky	Wythe thickness (in mm)	102	152	203	254	305
Date or ease from	0.0004	FRAME WALLS					Density of	Density of and (16.49 kN/m²)	1 53	2.15	3.21	4 02	88
Treatment to an early of an	60000	Extenior stud walls					Density of	Density of unit (19 64 kN/m²)	1 82	282	3.78	4 79	3.79
	900 0	Strain v 107 mm &	Slows - 107cm 63 406cm Thum neasons mediated Bonn edone	61 battlusm uns	andan sudan	0.53	Density of	Density of any (2, 21 kN/m²)	%	3.02	4 12	517	627
Hywdod (per am meeress)	000	© march v march	Street a lettered & second, terms 5/1/2001 measured, terms second Street at 15 and 10 and each and action	or transfer to	nom stekner	0.57							
right instruction, 15 time	5 6	Summer of summer	Topical Comments (S.)		i)	200							
Skylight metal frame, 10 mm wife glass	60.0	EXTERIOR SING WHILE WITH DITCK VEHICLE	WILL DEICK VEHICE			9 6							
Slate, 5 mm	0 34	Windows, glass, frame and sash	me and sash			38.0							
Sinte 6 mm	0 48												
Waterproofing membranes													
Bitumingus, gravel-covered	0.76												
Bitummous smooth surface	0 0 0												
	0.04												

Table C3-2 Minimum Densities for Design Loads from Materials

	Viinimum Densines for	Design Loads from Materials	
Мајепа)	Load (Ib-ft³)	Matenal	Load (Ib/fi3)
Aluminum	0יו	Lead	710
Binuminous products		Lime	
Asphaltum	91	Hydrated Toose	32
Graphite	133	Hydrated, compacted	45
Paratin	36	Masonn, Ashlar Stone	
Petroleum, crude	>5	Granne	165
Petroleum, refined	50	Limestone crystalline	165
Petroleum benzine	46	Limestone, coline	135
Petroleum, gasoline	42	Marble	173
Prich	69	Sandstone	144
Tar	75	Masonry, Brick	
Brass	526	Hard (low absorbtion)	130
Bronze	552	Medium (medium absorbtion)	115
Cast-stone masonry (cement, stone sand)	144	Soft (high absorbtion)	100
Cement, portland loose	90	Masonry, Concrete*	
Ceramic tile	150	Lightweight units	105
Charcoal	13	Medium weight units	125
Cinder fill	57	Normal weight units	135
Cinders, dry, in bulk	\$ 5	Masonry Grout	140
Coal		Masonry Rubble Stone	
Anthracite, piled	52	Granite	153
Biruminous ciled	47	Limesione crystalline	147
Lignite, piled	47	Limestone oolitic	138
Peat dry pited	23	Marble	156
Concrete plain		Sandstone	137
Cinder	108	Mortas cement or lime	130
Expanded-slag aggregate	100	Particleboard	45
Havdite (burned-glav aggregate)	90	Plywood	36
Slag	132	Riprap (Not submerged)	30
Stone (including grave)	144	Liniestone	83
Verniculate and perlite aggregate monload-bearing	25-50	Sandstone	90
Other light aggregate Toad-bearing	10-105	Sand	90
Concrete Reinforced	4-103	Clean and dry	90
Cinder Cinder	114	Ruser dry	106
Slag	138	Slag	100
Stone (including gravel)	150	Bank	70
Copper	556	Bank screenings	108
Cork compressed	14	Machine	95
·	17	Sand	
Earth (not submerged)	63	Slate	52 172
Clay, dry	110		
Clay, damp		Steel, cold-drawn	492
Clay and gravel, dry	100 78	Stone, Quarried, Piled	64
Silt, moist, loose		Basait, granie gneiss	96
Silt moist backed	96	Limestone marble, quartz	95
Silt, flowing	108	Sandstone	82
Sand and gravel, dry loose	100	Shale	92
Sand and gravet, dry packed	110	Greenstone homblende	107
Sand and gravel, wet	120	Terra Cotta, Architectural	
Earth (submerged)		Voids filled	120
Clay	80	Voids unfilled	72
Soil	70	Tin	459
River mud	90	Water	
Sand or gravel	60	Fresh	62
Sand or gravel and clay	6>	Sea	64
Glass	160	Wood, Seasoned	
Gravel, 🗗	104	Ash, commercial white	41
Gypsum loose	70	Cypress, southern	34
Gypsum, wallboard	50	Fir Douglas, coast region	34
lce .	57	Hem fir	28
Iron		Oak, commercial reds and whites	47
Cast	450	Pine, southern yellow	37
Wrought	48	Redwood	28
		Spruce red, white, and Stika	29
		Western hemlock	32
		Zinc rolled sheet	449

^{*}Tabulated values apply to solid masonry and to the solid portion of holiow masonry

Table C3-2 Minimum Densines for Design Loads from Materials

	Minimum Densities for D	esign Loads from Materials
	Load	
Malenal	(kN/m³)	Material
Aluminum	170	Lead
Bituminous products	13.7	Lime
Asphaltum	12.7	Hydrated, loose
Graphite	21 2	Hydrated, compacted
Parafin	8 8	Masonry, Ashlar Stone
Petroleum, crude	86	Granite
Petroleum, refined	79	Limestone, crystailine
Petroleum, benzine	72	Limestone colitic
Petroleum, gasoline	6.6	Marble
Pitch	10 8	Sandstone
Tar	11.8	Masonry, Brick
Brass	82.6	Hard (low absorbtion)
Bronze	86.7	Medium (medium absorbnon)
Cast-stone masonry (cement, stone, sand)	22 6	Soft (high absorbtion)
Cement, portland, loose	14.1	Masonry, Concrete*
Ceramic ble	23 6	Lightweight units
Charcoal	1.9	Medium weight units
Cinder fill	90	Normal weight units
Cinders, dry, in bulk	7 1	Masonry Grout
Coal	_ +	Masonry, Rubble Stone
Anthracite, piled	8.2	Granite
Bituminous, piled	7 4	Limestone, crystalline
Lignite, piled	7.4	Lamestone, online
Peat, dry, piled	3.6	Marble
Concrete, plain		Sandstone
Cinder	17 O	Mortar, cement or hime
Expanded-slag aggregate	15.7	Particleboard
Haydite (burned-clay aggregate)	14.1	Piywood
Slag	20 7	Raprap (Not submerged)
Stone (including gravei)	22 6	Limestone
Vermiculite and perlite aggregate, nonload-bearing	39-79	Sandstone
Other light aggregate, load-bearing	11 0-16 5	Sand
Concrete, Reinforced		Clean and dry
Cinder	17.4	River, dry
Stag	21 7	Stag
Stone (including grave!)	23.6	Bank
Copper	87 3	Bank screenings
Cork, compressed	2.2	Machine
Earth (not submerged)		Sand
Clay, dry	99	Siate
Clay, damp	17.3	Steel, cold-drawn
Clay and grave) dry	15.7	Stone, Quarned, Piled
Silt, moist, loose	12.3	Basalt, granite, gueiss
Silt, moist, packed	15 1	Limestone, marble, quartz
Silt, flowing	17 0	Sandstone
Sand and gravel, dry, loose	15 7	Shale
Sand and gravel dry, packed	17.3	Greenstone, homblende
Sand and gravel, wet	189	Terra Cotta, Architectural
Earth (submerged)	•• ,	Voids filled
Clay	12.6	Voids unfilled
Soil	11.0	Tin
River mud	14 1	Water
Sand or gravel	94	Fresh
Sand or gravel and clay	10.2	Sea
Glass	25.1	Wood, Seasoned
Gravel, dry	16.3	Ash, commercial white
	11.0	Cypress, southern
Gypsum, loose Gypsum, wallboard	7,9	Cypress, southern Fir, Douglas, coast region
. **		· -
ice (9.0	Hem fir
Iron Com	70.7	Oak, commercial reds and whites
Cass Westerness	70.7	Pine, southern yellow
Wrought	75.4	Redwood
		Spruce, red, white, and Stika
		Western hemlock
		Zinc, rolled sheet

^{*}Tabutated values apply to solid masonry and to the solid portion of hollow masonry

C4. Live Loads

C4.2 Uniformly Distributed Loads

C4.2.1 Required Live Loads. A selected list of loads for occupancies and uses more commonly encountered is given in 4.2.1, and the authority having jurisdiction should approve on occupancies not mentioned. Tables C4-1 and C4-2 are offered as a guide in the exercise of such authority.

In selecting the occupancy and use for the design of a building or a structure, the building owner should consider the possibility of later changes of occupancy involving loads heavier than originally contemplated. The lighter loading appropriate to the first occupancy should not necessarily be selected. The building owner should ensure that a live load greater than that for which a floor or roof is approved by the authority having jurisdiction is not placed, or caused or permitted to be placed, on any floor or roof of a building or other structure.

In order to solicit specific informed opinion regarding the design loads in Table 4-1, a panel of 25 distinguished structural engineers was selected. A Delphi [1] was conducted with this panel in which design values and supporting reasons were requested for each occupancy type. The information was summarized and recirculated back to the panel members for a second round of responses, those occupancies for which previous design loads were reaffirmed, as well as those for which there was consensus for change, were included

It is well known that the floor loads measured in a live-load survey usually are well below present design values [2,3,4,5]. However, buildings must be designed to resist the maximum loads they are likely to be subjected to during some reference period T, frequently taken as 50 years Table C4-2 briefly summarizes how load survey data are combined with a theoretical analysis of the load process for some common occupancy types and illustrates how a design load might be selected for an occupancy not specified in Table 4-1 [6] The floor load normally present for the intended functions of a given occupancy is referred to as the sustained load. This load is modeled as constant. until a change in tenant or occupancy type occurs. A live-load survey provides the statistics of the sustained load. Table C4-2 gives the mean, m., and standard deviation, σ_s , for particular reference areas. In addition to the sustained load, a building is likely to be subjected to a number of relatively short-duration, high-intensity, extraordinary or transient loading events (due to crowding in special or emergency circumstances, concentrations during remodeling, and the like). Limited survey information and theoretical considerations lead to the means, m., and standard deviations, o., of single transient loads shown in Table C4-2

Combination of the sustained load and transient load processes, with due regard for the probabilities of occurrence, leads to statistics of the maximum total load during a specified reference period T. The statistics of the maximum total load depend on the average duration of an individual tenancy, τ , the mean rate of occurrence of the transient load, v_e , and the reference period, T. Mean values are given in Table C4-2. The mean of the maximum load is similar, in most cases, to the Table 4-1 values of minimum uniformly distributed live loads and, in general, is a suitable design value.

C4,3 Concentrated Loads

C4.3.1 Accessible Roof-Supporting Members. The provision regarding concentrated loads supported by roof trusses or other primary roof members is intended to provide for a common situation for which specific requirements are generally lacking

C4.4 Loads on Handrails, Guardrail Systems, Grab Bar Systems and Vehicle Barrier Systems

C4.4.2 Loads

- (a) Loads that can be expected to occur on handrail and guardrail systems are highly dependent on the use and occupancy of the protected area. For cases in which extreme loads can be anticipated, such as long straight runs of guardrail systems against which crowds can surge, appropriate increases in loading shall be considered.
- (b) When grab bars are provided for use by persons with physical disabilities the design is governed by CABO A117 Accessible and Usable Buildings and Facilities
- (c) Vehicle barrier systems may be subjected to horizontal loads from moving vehicles. These horizontal loads may be applied normal to the plane of the barrier system, parallel to the plane of the barrier system, or at any intermediate angle. Loads in garages accommodating trucks and buses may be obtained from the provisions contained in Standard Specifications for Highway Bridges, 1989. The American Association of State Highway and Transportation Officials
- (d) This provision is introduced to the standard in 1998 and is consistent with the provisions for stairs
- (e) Side rail extensions of fixed ladders are often flexible and weak in the lateral direction. OSHA (CFR 1910) requires side rail extensions, with specific geometric requirements only. The load provided is introduced to the standard in 1998, and has been determined on the basis of a 250 lb. person standing on a rung of the ladder, and accounting for reasonable angles of pull on the rail extension.

C4.6 Partial Loading. It is intended that the full intensity of the appropriately reduced live load over portions of the structure or member be considered, as well as a live load of the same intensity over the full length of the structure or member.

Partial-length loads on a simple beam or truss will produce higher shear on a portion of the span than a full-length load. 'Checkerboard' loadings on multistoried, multipanel bents will produce higher positive moments than full loads, while loads on either side of a support will produce greater negative moments. Loads on the half span of arches and domes or on the two central quarters can be critical. For roofs, all probable load patterns should be considered. Cantilevers cannot rely on a possible live load on the anchor span for equilibrium.

C4.7 Impact Loads. Grandstands, stadiums, and similar assembly structures may be subjected to loads caused by crowds swaying in unison, jumping to its feet, or stomping. Designers are cautioned that the possibility of such loads should be considered

C4.8 Reduction in Live Loads

C4.8.1General. The concept of, and methods for, determining member live load reductions as a function of a loaded member's influence area, A_F was first introduced into this standard in 1982 and was the first such change since the concept of live load reduction was introduced over 40 years ago. The revised formula is a result of more extensive survey data and theoretical analysis [7]. The change in format to a reduction multiplier results in a formula that is simple and more convenient to use. The use of influence area, now defined as a function of the tributary area, A_T , in a single equation has been shown to give more consistent reliability for the various structural effects. The influence area is defined as that floor area over which the influence surface for structural effects is significantly different from zero.

The factor K_{LL} is the ratio of the influence area (A_f) of a member to its tributary area (A_f) , i.e. $K_{LL} = A/A_f$, and is used to better define the influence area of a member as a function of its tributary area. Fig. C4 illustrates typical influence areas and tributary areas for a structure with regular bay spacings. Table 4-2 has established K_{LL} values (derived from calculated K_{LL} values) to be used in Eq. 4-1 for a variety of structural members and configurations. Calculated K_{LL} values vary for column and beam members having adjacent cantilever construction, as is shown in Fig. C4, and the Table 4-2 values have been set for these cases to result in live load reductions which are slightly conservative. For unusual shapes, the concept of significant influence effect should be applied

An example of a member without provisions for

continuous shear transfer normal to its span would be a precast T-beam or double-T beam which may have an expansion joint along one or both flanges, or which may have only intermittent weld tabs along the edges of the flanges. Such members do not have the ability to share loads located within their tributary areas with adjacent members, thus resulting in $K_{\rm LL}$, = 1 for these types of members.

Reductions are permissible for two-way slabs and for beams, but care should be taken in defining the appropria influence area. For multiple floors, areas for members supporting more than one floor are summed.

The formula provides a continuous transition from unreduced to reduced loads. The smallest allowed value c the reduction multiplier is 0.4 (providing a maximum 60° reduction), but there is a minimum of 0.5 (providing a 50° reduction) for members with a contributory load from jus one floor.

C4.8.2 Heavy Live Loads. In the case of occupancies involving relatively heavy basic live loads, such as storag buildings, several adjacent floor panels may be fully loaded. However, data obtained in actual buildings indica that rarely is any story loaded with an average actual live load of more than 80% of the average rated live load. It appears that the basic live load should not be reduced for the floor-and-beam design, but that it could be reduced a flat 20% for the design of members supporting more than one floor. Accordingly, this principle has been incorporated in the recommended requirement.

C4.9 Minimum Roof Live Loads

C4.9.1 Flat, Pitched, and Curved Roofs. The values specified in Eq.4-1 that act vertically upon the projected area have been selected as minimum roof live loads, even in localities where little or no snowfall occurs. This is because it is considered necessary to provide for occasion loading due to the presence of workers and materials during repair operations.

C4.9.2 Special Purpose Roofs. Designers should conside any additional dead loads that may be imposed by saturat landscaping materials. Special purpose or occupancy roof live loads may be reduced in accordance with the requirements of Section 4.8

C4.10 Crane Loads. All support components of moving bridge cranes and monoral cranes, including runway beams, brackets, bracing, and connections, shall be designed to support the maximum wheel load of the crane and the vertical impact, lateral, and longitudinal forces induced by the moving crane. Also, the runway beams shall be designed for crane stop forces. The methods for determining these loads vary depending on the type of

crane system and support. References [8 through 11] describe types of bridge cranes and monoral cranes. Cranes described in these references include top running bridge cranes with top running trolley, underhung bridge cranes, and underhung monoral cranes. Reference [12] gives more stringent requirements for crane runway design that are more appropriate for higher capacity or higher speed crane systems.

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- [11] Metal Building Manufacturers Association. Low Rise Building Systems Manual, 1986, MBMA, Inc., Cleveland OH
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Lable C4-1 Minimum Uniformly Distributed Live Loads

Occupancy or use	Live Load lb/ft² (kN/m²)	Occupancy or use	Live Load B/ft² (kN/n		
Air-conditioning (machine space)	200* (9 58)	Laboratories, scientific	100 (4 79		
Amusement park structure	100* (4 79)	Laundries	150* (7.1)		
Attic Nonresidential		Libranes, corridors	80* (3.83		
Nonstorage	25 (1 20)	Manufacturing, ice	300 (14 3)		
Storage	80* (3 83)	Morgue	125 (6.00		
Bakery	150 (7.18)	Office Buildings			
Exterior	100 (4 79)	Business machine equipment	100* (4.79		
Interior (fixed seats)	60 (2 87)	Files (see file room)			
interior (movable seats	100 (4,79)	Printing Plants			
Boathouse, floors	100* (4.79)	Composing rooms	100 (4.79		
Boiler room, framed	300* (14 36)	Linetype rooms	100 (4.79		
Droadcasting studio	100 (4 79)	Paper storage			
Catwalks	25 (1.20)	Press rooms	150* (7.1)		
Ceiling, accessible funed	10# (0.48)	Public rooms	100 (4 79		
Cold Storage		Railroad tracks	‡‡		
No overhead system	250‡ (1197)	Ramps			
Overhead system		Driveway (see garages)			
Floor	150 (7 (8)	Pedestrian (see sidewalks and corridors in Table 2)			
Roof	250 (11 97)	Seaplane (see hangars)			
Computer equipment	150* (7.18)	Rest rooms	60 (2.87		
Courtrooms	50 - 100 (2 40 - 4 79)	Rinks			
Dormitanes	,	Ice Skating	250 (11 9		
Nonpartnioned	80 (3 \$3)	Roller skating	100 (4.79		
Partitioned	40 (1 92)	Storage, hay or grain	300* (143		
Elevator machine room	150* (7.18)	Telephone exchange	150* (7 1		
Fan room	150* (7.18)	Telephone exchange 150° Theaters			
File room		Dressing rooms	40 (1 92		
Duplicating equipment	150* (7.18)	Grid-iron floor or fly gallery			
Card	125* (6 00)	Grating	60 (2.87		
Letter	80* (3.83)	Well beams 250 lb/ft per pair			
Foundries	600* (28 73)	Header beams, 1000 lb/ft			
Fuel rooms, framed	400 (19.15)	Pin rail, 250 lb/ft			
Garages - trucks	§	Projection room	100 (4 7		
Greenhouses	150 (7 18)	Toilet rooms	60 (2.87		
Hangars	150§ (7-18)	Transformer rooms	200* (9.5		
Incinerator charging floor	100 (4 70)	Vaults, in offices	250* (11 '		
Kitchens, other than domestic	150* (7 18)				

^{*} Use weight of actual equipment or stored material when greater

[‡] Plus 150 (b/ft² (7 18 kN/m²) for trucks.

[§] Use American Association of State Highway and Transportation Officials lane loads. Also subject to not less than 100% maximum axle load.

** Paper storage 50 lb/ft (2 40 kN/m²) of clear story height

^{##} As required by railroad company.

[#] Accessible ceilings normally are not designed to support persons. The value in this table is intended to account for occasional light storage or suspension of items. If it necessary to support the weight of maintenance personnel, this shall be provided for.

Table C4-2 **Typical Live Load Statistics**

	Surve	y Load	Transie	nt Load	Теп	nporal Constants		Mean
Occupancy or use	m, lb/ft² (kN/m²)	σ, " ιb/ft² (kN/m²)	m _i * lb/ft² (kN/m²)	σ * lb/ft² (kN/m²)	رب† (years)	v₊‡ (peryear)	T§ (years	maximum load* lb/ft- (kN/m²)
Office buildings								_
offices	10 9 (0 52)	5 9 (0 28)	8.0 (0 38)	8 2 (0 39)	8	1	50	55 (2 63)
Residential								
renter occupied	6 0 (0 29)	2.6 (0.12)	6.0 (0.29)	6 6 (0 32)	2	3	50	36 (1.72)
owner occupied	6.0 (0.29)	2.6 (0 12)	6 0 (0 29)	6 6 (0.32)	10	1	50	38 (1 82)
Hotels								
guest rooms	4 5 (0 22)	1 2 (0 06)	6 0 (0 29)	5 \$ (0.28)	5	20	50	46 (2.2)
Schools								
classrooms	12 0 (0 57)	2.7 (0.13)	6 9 (0 33)	$3 \neq (0.16)$	J	1	100	34 (1 63)

For 200-ft² (18 58 m²) area, except 1000 ft² (92 9 m²) for schools
 † Duration of average sustained load occupancy
 ‡ Mean rate of occurrence of transient load

[§] Reference period.